

# VESTAS SAILROCKET

AND DEVELOPMENTS IN HIGH SPEED SAILING

Malcolm Barnsley

May 2011



# THE CUSP OF A REVOLUTION?

- MULTIS AND MONOS REACHING END OF LINE
- CAVITATION A REAL BARRIER 50+K
- HYDROFOILS WIDELY ADOPTED BUT ON CRAFT WITH SEVERE LIMITATIONS

THE BASIS FOR THIS REVOLUTION IS EXPLAINED  
IN THE STORY BELOW. I COULD BE WRONG –  
SEE WHAT YOU THINK!

# BLANK CANVAS - WHAT FORM?

WHY SPEED SAILING?

CUTTING EDGE  
DEVELOPMENT

WIDER APPLICATIONS

?

FUN IS A SERIOUS BUSINESS



# MANY DIFFERENT SOLUTIONS [2000]



# MOTH & HOBIE TRIFOILER CLASS HAS ESTABLISHED PRACTICALITY OF FOIL BORNE CRAFT

NOT TARGETING  
RECORDS  
BUT CAPABLE OF  
28 KNOTS



LONGSHOT 43 KNOTS  
HOBIE PRODUCTION VERSION 32 KNOTS



# EARLY DAYS – NEWNHAM COMMON 1973



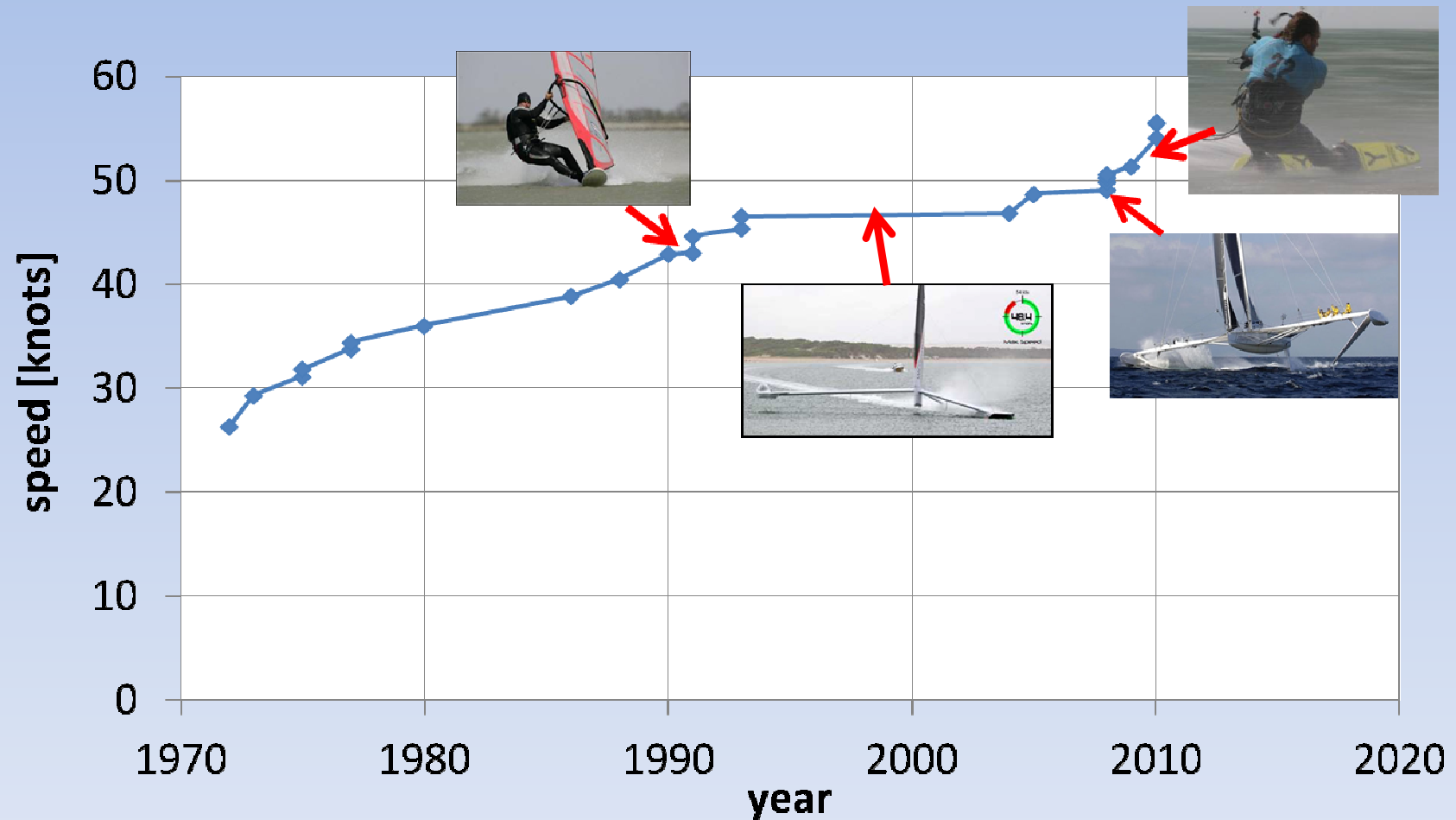
**FIRST OFFICIAL WORLD SAILING SPEED  
RECORD ESTABLISHED**

# THE WSSRC RULES

- 500m one way course
- NO DESIGN RESTRICTIONS
- No restriction on wind strength or direction
- Unlimited run up
- No towing during run up
- No stored power ie batteries, compressed air; fuel
- Parts of the boat may be jettisoned during the run
- Must carry a minimum of 1 person

# OUTRIGHT 500m RECORD 1973-2010

## 26.3-55.6 KNOTS





# HIGH SAILFORCE/WEIGHT NEEDED FOR HIGH EFFICIENCY

HIGH SPEED (RELATIVE TO WIND) DEMANDS LOW APPARENT WIND ANGLE (EG 23 DEGREES FOR 50K IN 22K)



LOW APPARENT WIND ANGLE REQUIRES HIGH AERO AND HYDRO L/D RATIOS (MEASURED HORIZONTALLY)



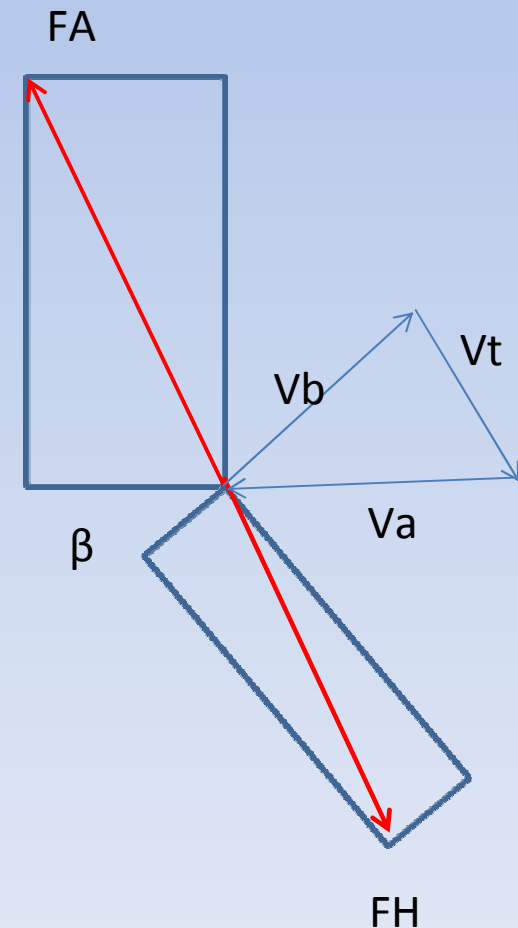
HIGH L/D HYDRODYNAMICALLY REQUIRES THE L/D OF A GOOD HIGH AR FOIL



AS THE DRAG DUE TO PAYLOAD HAS TO BE ADDED THIS LOWERS THE L/D A LOT.

**HIGH L/D CAN STILL BE ACHIEVED IF THE FOIL LIFT IS LARGE RELATIVE TO THE BUOYANT LIFT OR CRAFT WEIGHT**

**THEN THE EFFECT OF PAYLOAD DRAG IS DIMISHED**



# GRAVITY BASED STABILITY

MAX RIGHTING MOMENT  
PROPORTIONAL TO MASS X BEAM

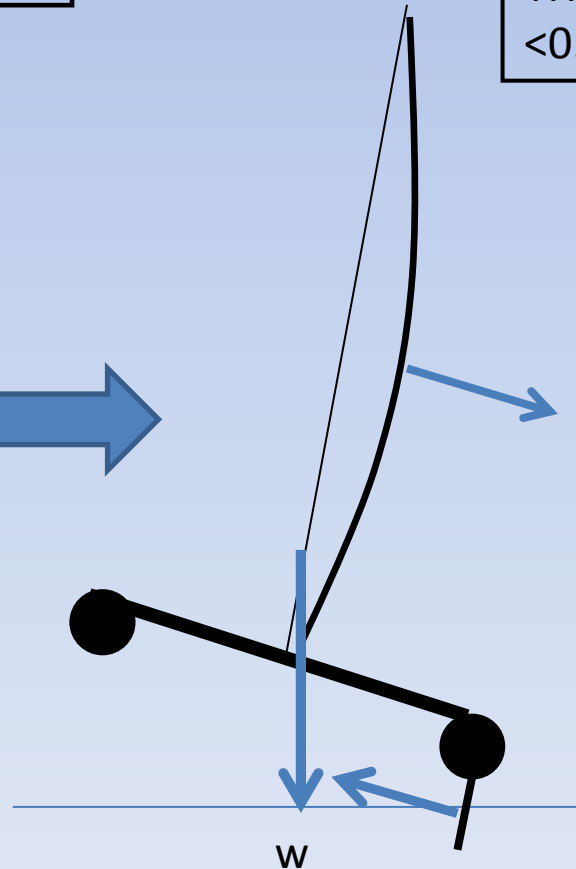
SAILFORCE/WEIGHT  
< 0.5  
THRUST/WEIGHT  
< 0.05

HYDRODRAG  
PROPORTIONAL TO  
MASS

THRUST TO  
DRAG RATIO  
INHERENTLY  
LIMITED

AERO DRAG PROPORTIONAL TO  
BEAM

BEAM LIMITED  
TO 0.8-1.0L



# DISPLACEMENT MULTIHULLS

- Sail sized so stability limit reached at same  $V_t$
- Weight proportional to  $L^3$
- Wetted area proportional to  $L^2$
- Max RM proportional to  $L^4$
- Height of rig proportional to  $L$



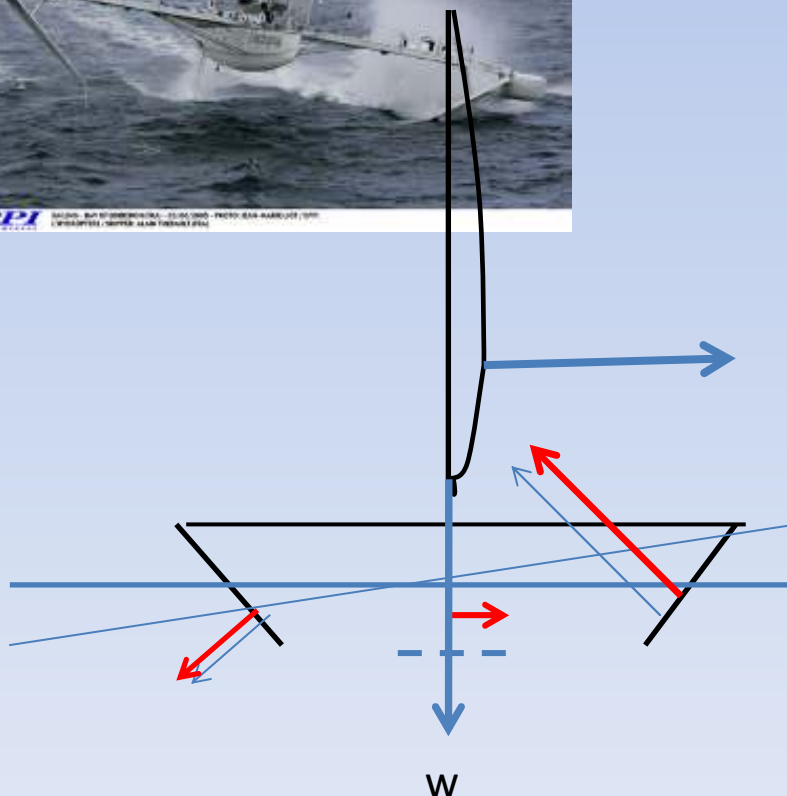
SPEED PROPORTIONAL TO  
SQUARE ROOT L

+BANC POPULAIRE 60 F 24HR

\*BANC POPULAIRE 40M 24HR

LENGTH [m]	SPEED [MAX knots]	[AV knots]	COST [million \$]
10	26		0.1
20	37	+ [28]	2.0
30	45		8.0
40	52	* [38]	20.0
50	58		30.0

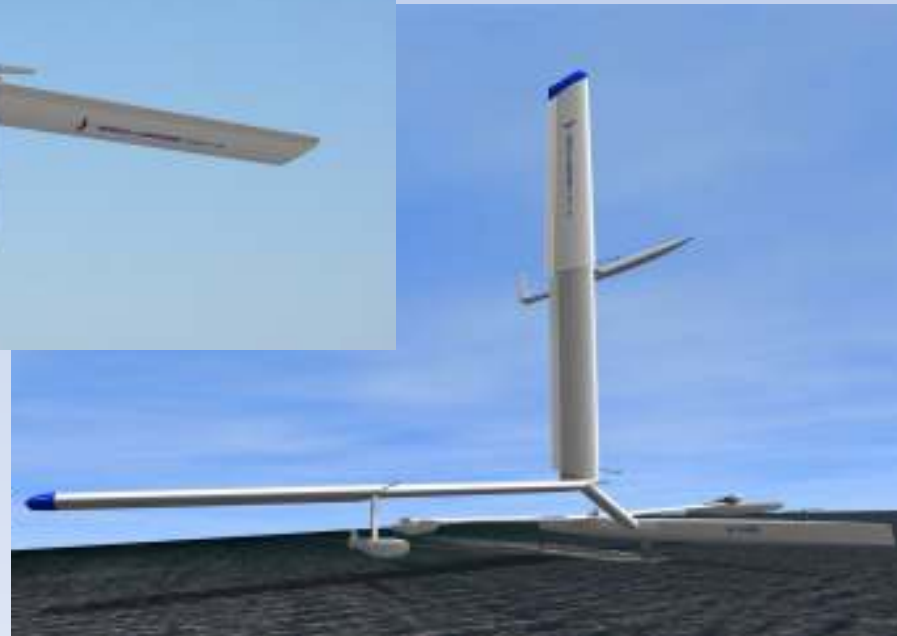
# WIDELY USED SYMMETRIC SURFACE PIERCING FOIL CONFIGURATION



- VERY COMPLEX
- ROLL/HEAVE STABILITY NOT WELL DEFINED
- DIRECTION OF FORCE ON WW FOIL CHANGES
- IMMERSION OF BOTH FOILS CONTANTLY CHANGES
- REALLY NEEDS CONTROL OF INDIVIDUAL PITCH ANGLES
- VERY EFFICIENT WHEN WW FOIL IS JUST UNLOADED OR FLOWN CLEAR
- T FOIL SHARES SIDELOAD REACTION

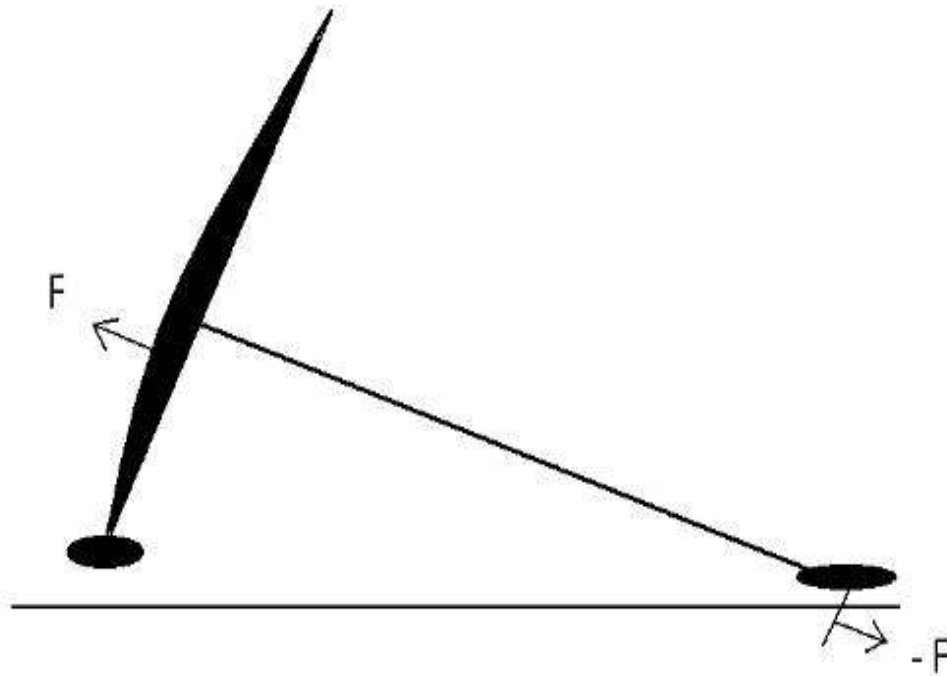
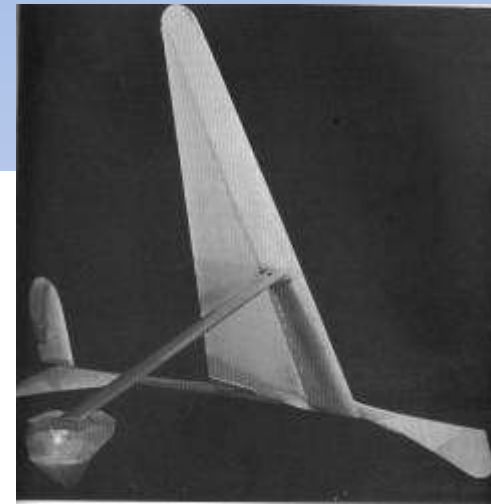
# V39 ALBATROSS

WING IN GROUND EFFECT STABILISED  
ROCK OVER FOR TACKLING



# SMITH ELEGANT BUT NEGLECTED SOLUTION

- Transverse forces balance each other exactly
- Fore/aft moments very nearly balance



# 2 CONCEPTS WITH NO CLEARLY DEFINED SAIL LOAD LIMITS

SYM FOILER

$$\mu = (1 + F') / 2F'$$

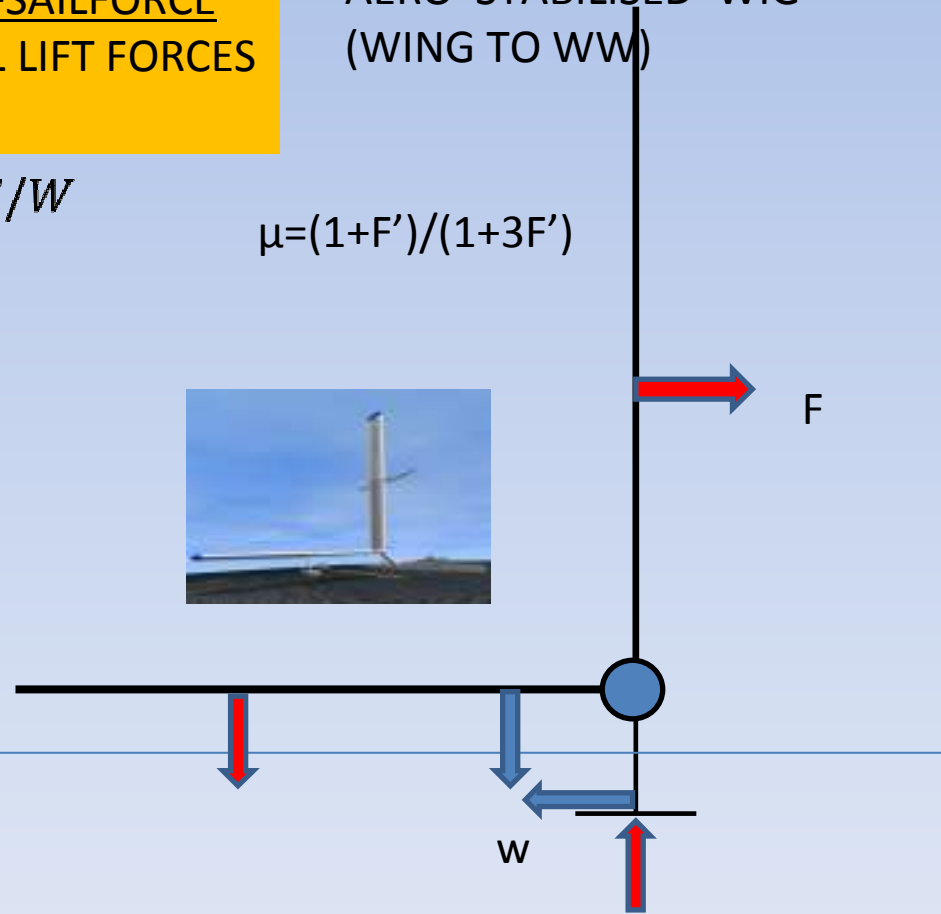
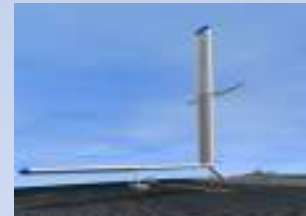


'INDUCED DRAG EFFICIENCY'  
 $\mu = \frac{\text{PAYLOAD} + \text{SAILFORCE}}{\text{SUM OF ALL LIFT FORCES}}$

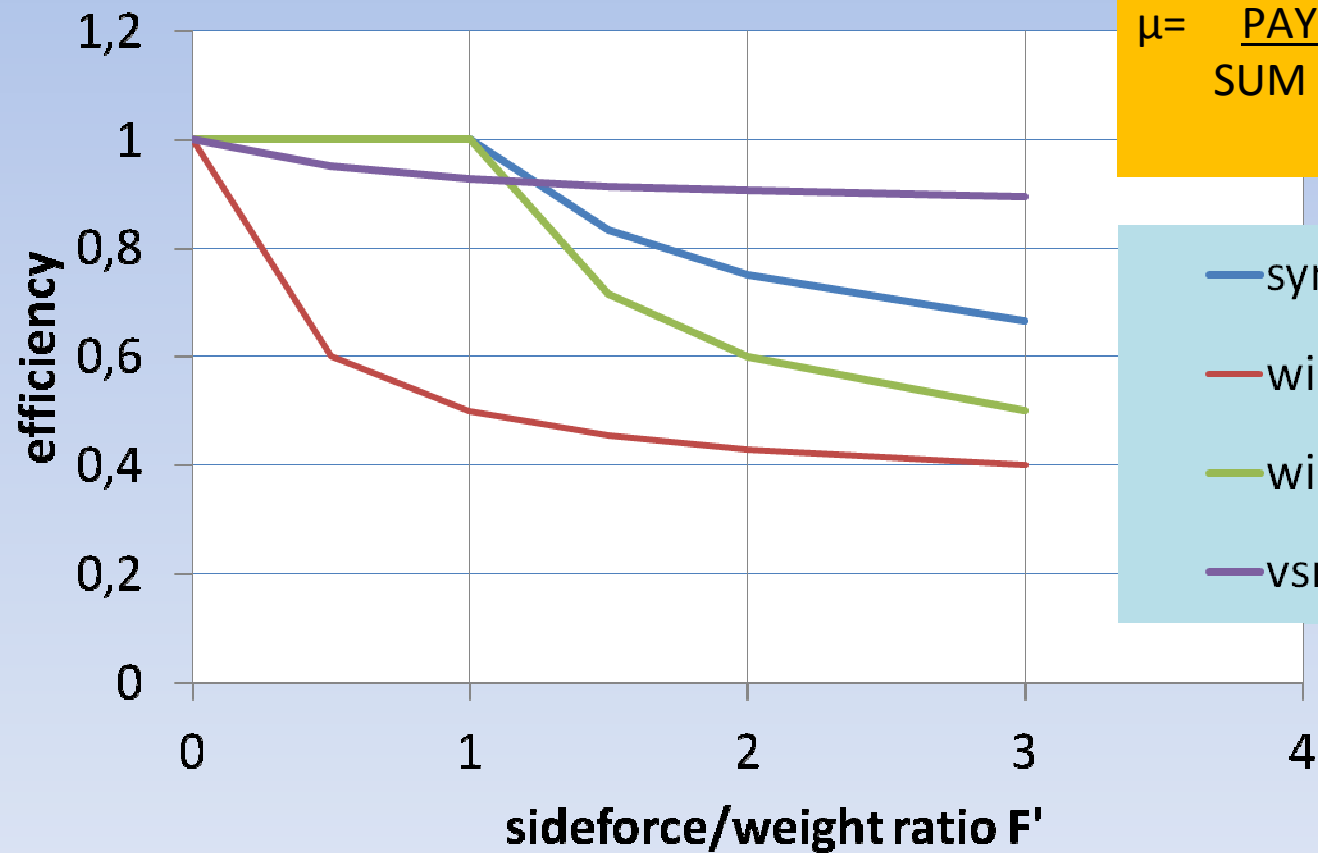
$$F' = F / W$$

AERO STABILISED WIG  
 (WING TO WW)

$$\mu = (1 + F') / (1 + 3F')$$



# EFFICIENCY ON THE BASIS OF INDUCED DRAG



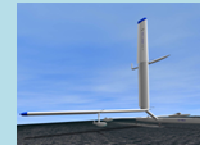
$$\mu = \frac{\text{PAYLOAD} + \text{SAILFORCE}}{\text{SUM OF ALL LIFT FORCES}}$$

— symfoiler



— wig ww

— wig lw



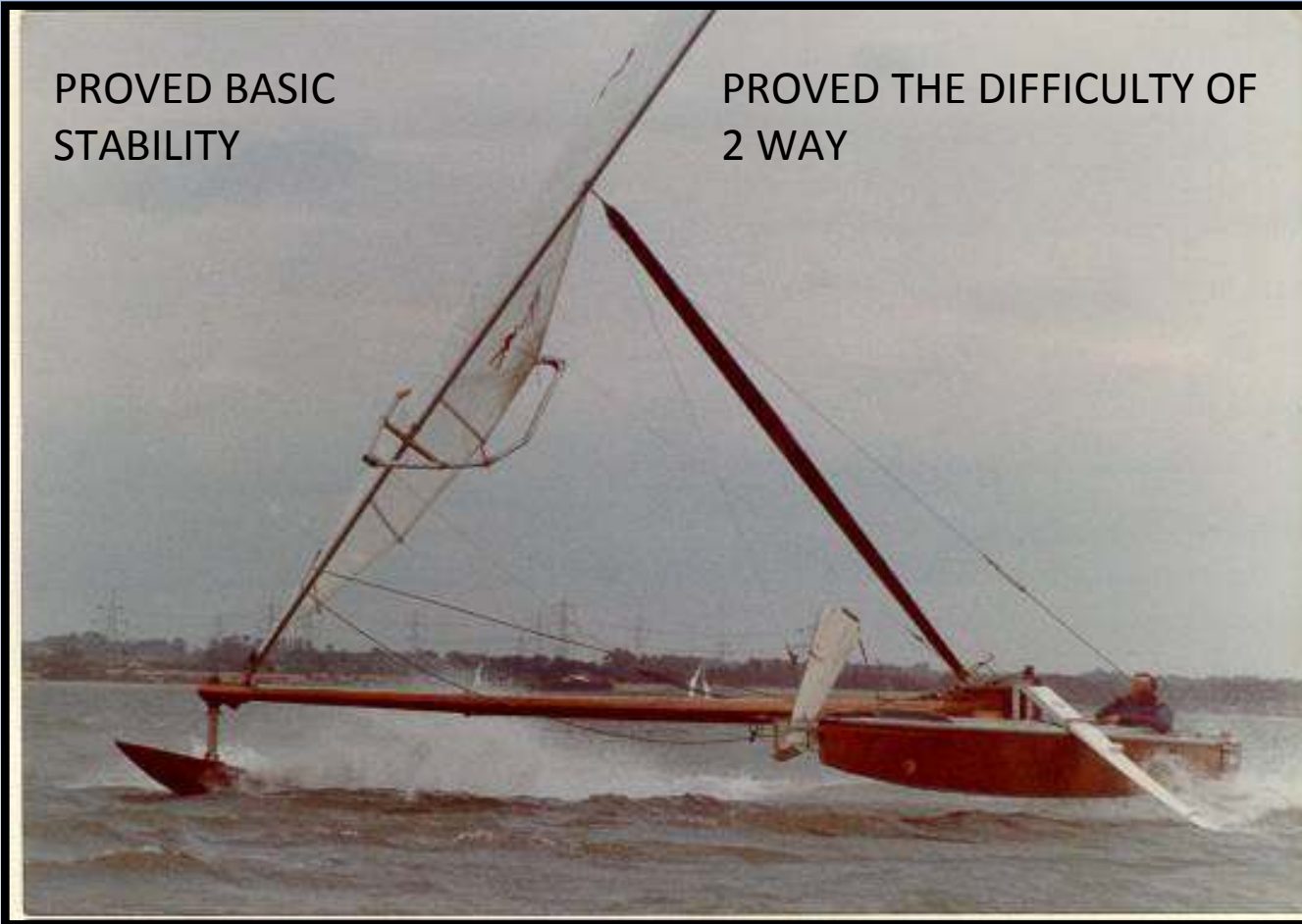
— vsr/smith type



# EARLY SMITH CONFIGURATION 1988

PROVED BASIC  
STABILITY

PROVED THE DIFFICULTY OF  
2 WAY



# EXPERIMENTS IN TEXAS 1989

LEEWARD FLOATS FREE TO YAW AND PITCH  
TWIN ROLLER HEADSAILS  
MAIN HULL VERTICAL DAGGER BOARDS  
25 KNOTS FULLY REVERSIBLE



## 1999 DESIGNED PLATFORM AND HULL FORM

- PRACTICAL PLATFORM
- VERY ADJUSTABLE GEOMETRY
- LOTS OF RESISTANCE TO PITCHPOLE



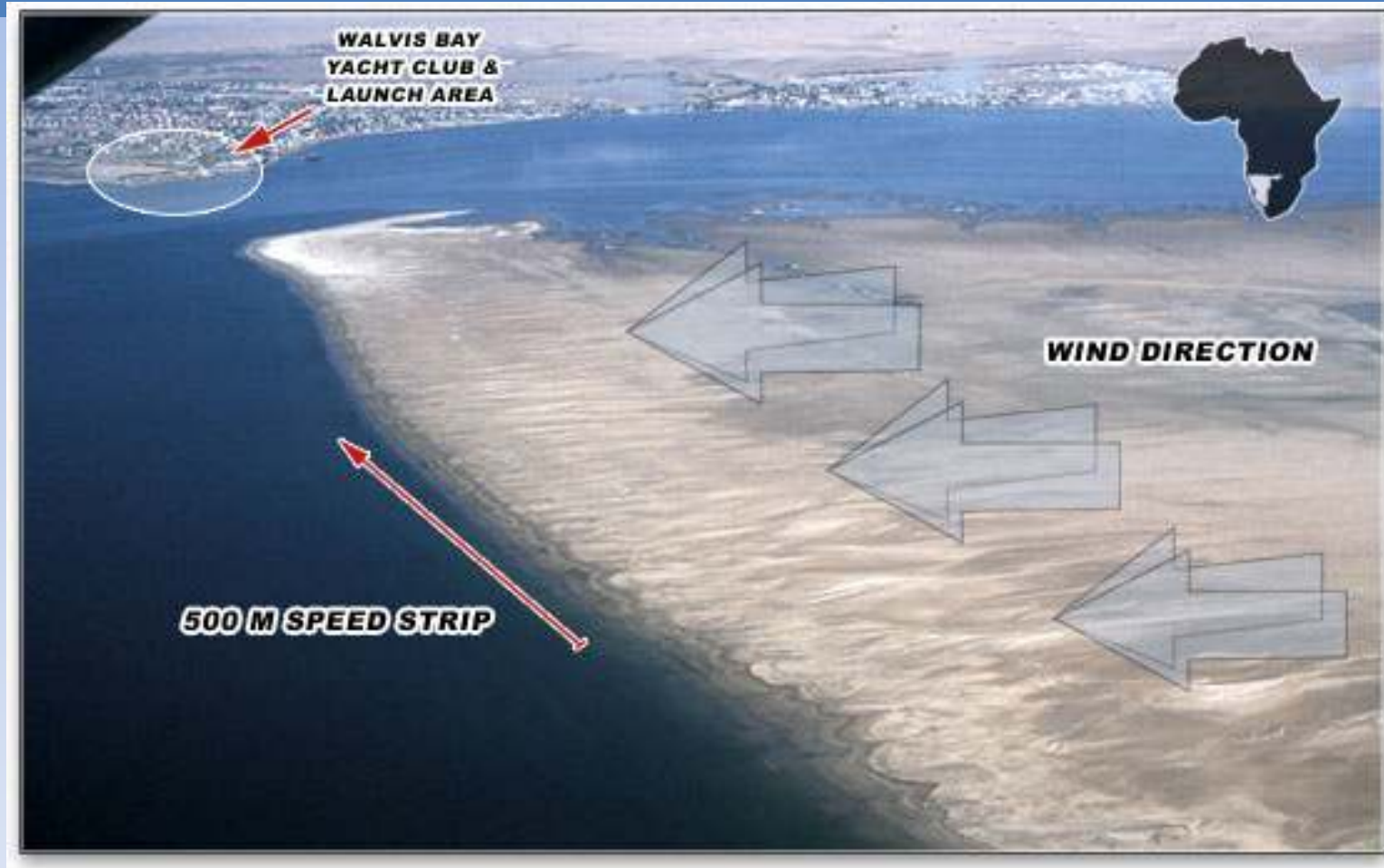
# LAUNCH SAILROCKET1 – APRIL 2004



# PROBLEM 1 – SOFT SAIL



# WALVIS BAY SPEED STRIP



## PROBLEM 2 - UNCONTROLLABLE ROUND UPS

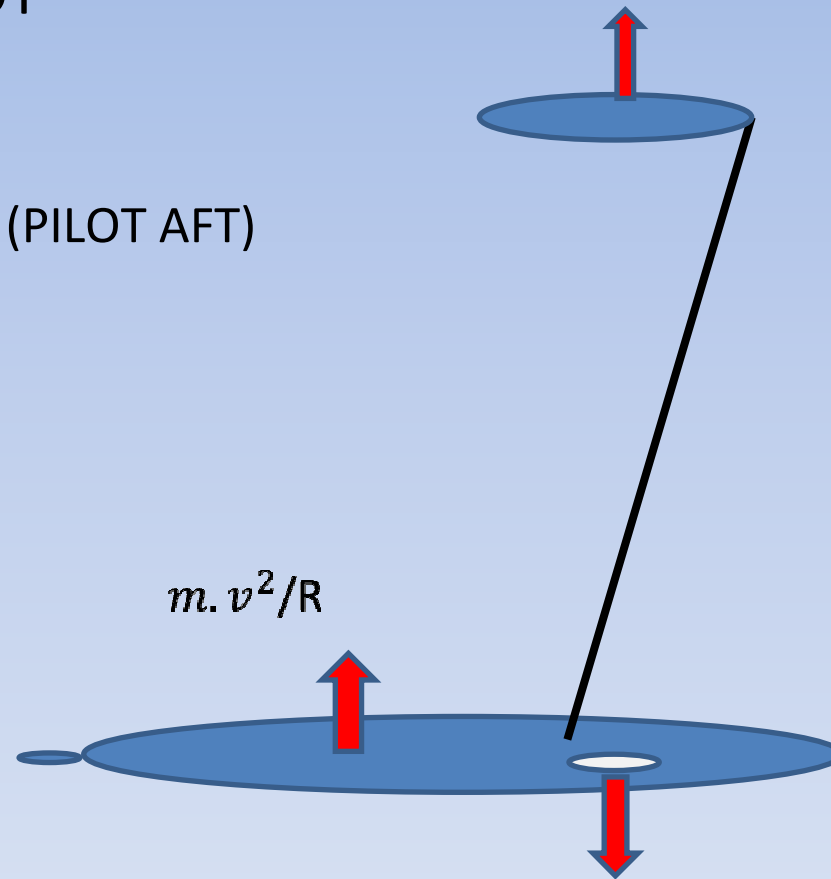
STATICALLY BALANCED BUT NOT  
DYNAMICALLY

### CAUSES

CENTRE OF MASS TOO FAR AFT (PILOT AFT)

NON FEATHERING WING

POOR RUDDER ACTUATION



40 KNOTS IN 17 KNOTS TRUE – LEEWARD POD STILL CONTACTING





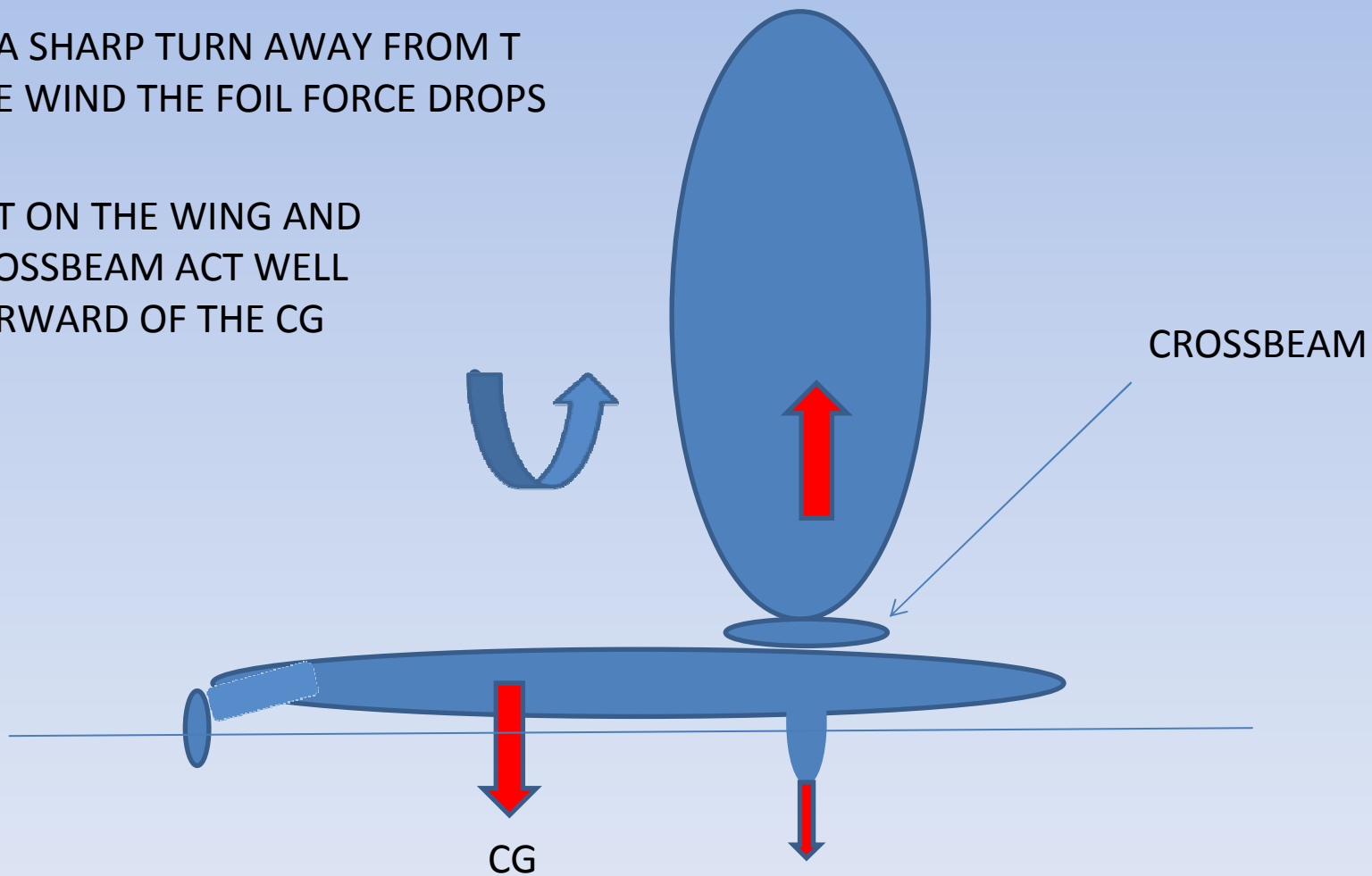
## PROBLEM 3 – TAKE OFF



## PROBLEM 3

IN A SHARP TURN AWAY FROM THE WIND THE FOIL FORCE DROPS

LIFT ON THE WING AND CROSSBEAM ACT WELL FORWARD OF THE CG



## SAILROCKET 1

DESIGNED	2000
DESIGN SPEED	50 KNOTS
LAUNCHED	2004
BEST RUN	49.3 KNOTS 2009



FASTEST RUN 49.3KNOTS (52 KNOTS PEAK )



# LIMITATIONS OF VSR1

- DIRECTIONALLY UNSTABLE OUTSIDE LIMITED RANGE
- PITCH UNSTABLE OUTSIDE A LIMITED RANGE
- C OF G TOO FAR AFT
- EFFECTS MADE WORSE BY NON FEATHERING WING
- SUBCAVITATING HYDROFOILS

# SUCCESSSES OF VSR1

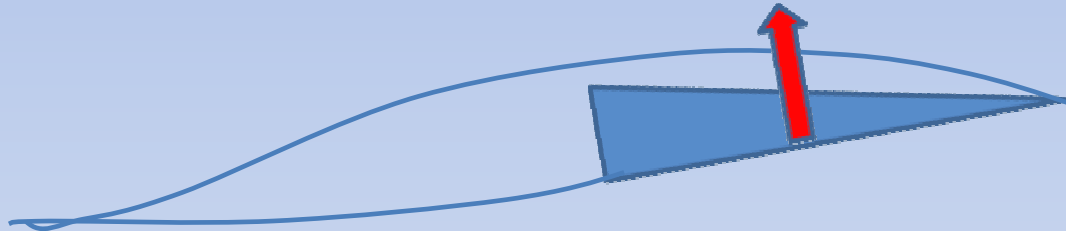
- ACHIEVED PREDICTED SPEEDS
- EXCEEDED ORIGINAL TARGET SPEED
- DEMONSTRATED ABILITY TO HARNESS HIGH POWER/WEIGHT
- DEMONSTRATED DIRECTIONAL STABILITY  
(SAILED ITSELF ON THE COURSE)

# BARRIERS TO THE 60'S

1. CAVITATION
  - steep rise in drag and very rapid deterioration of foil surface
  - Impossible to avoid at >55knots irrespective of  $C_l$  ( loading)
2. SUPERCAVITATING FOIL DRAG
  - Lower L/D than fully wetted foils – needs greater power/weight
3. LIMITED THRUST/STATIC STABILITY – particularly in relation to wetted area
4. ADDED DRAG DUE TO WAVES – particularly planing and displacement hulls

# CAVITATION & VENTILATION

- CAVIATION CAN NOT BE AVOIDED ABOVE 55 KNOTS EXCEPT BY PREVENTILATING THE LOW PRESSURE SURFACE



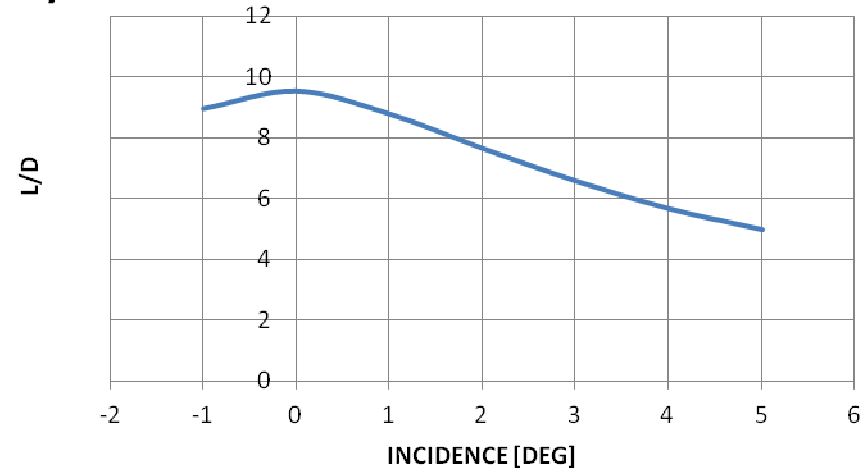
- THIS MEANS USING A SUPERVENTILATING FOIL OR INCLINED PLANING SURFACE (KITE BOARDS)



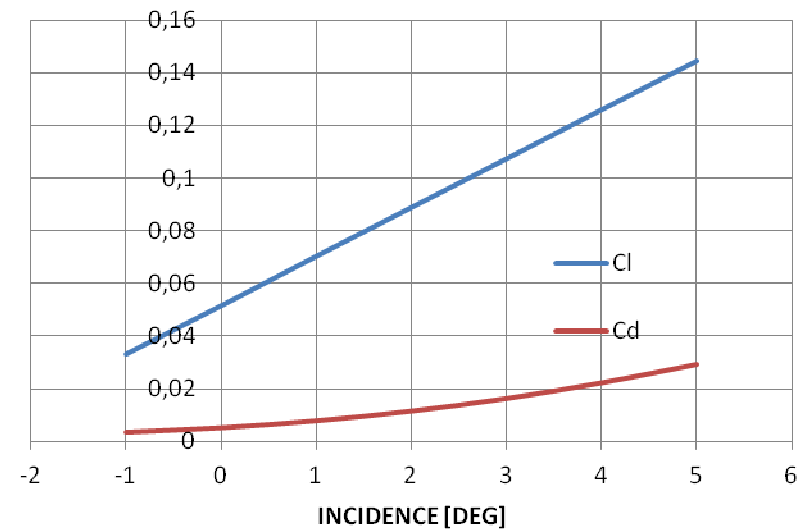
# SUPERVENTILATING PERFORMANCE

- LIFT SLOPE  $< \pi/2$

L/D 10% THICK CAMBERED WEDGE



- TULIN MAPPING FULLY WETTED TO FULLY VENTILATED
- L/D UP TO 10 3D AR3
- 10% THICK
- CAMBER OF PRESSURE FACE CRITICAL





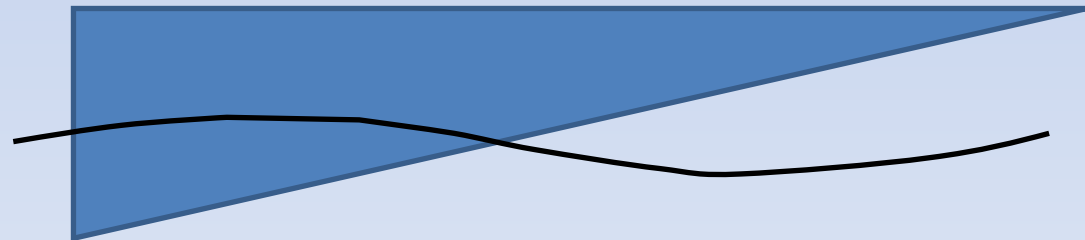
# PLANING ADDED DRAG IN WAVES

The following assumptions are used

- 1.The vertical motion of the craft is neglected
- 2.The apparent wave length is large compared to the wetted length
- 3.Savitski lift forces apply instantaneously
- 4.Prismatic single chine hull
- 5.No added spray drag component

$$z = z_0 \cdot \sin \omega t$$

$$\delta\alpha = \dot{z} / V_b$$



# PLANING ADDED DRAG IN WAVES

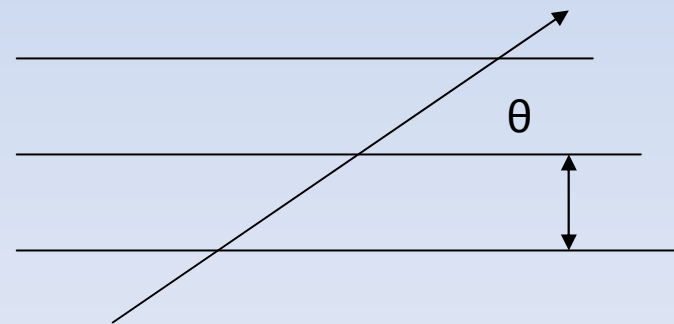
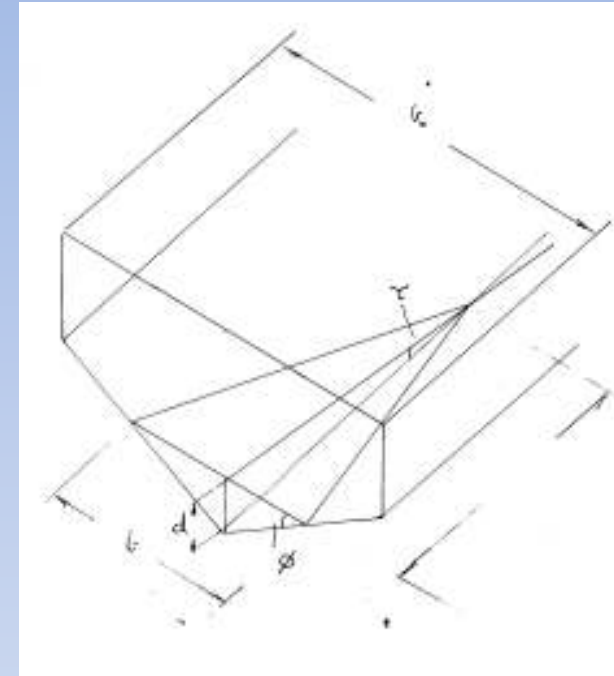
$$E = \int_0^T F \cdot dz = \int_0^T F \cdot \dot{z} \cdot dt$$

$$E = 0.5 \cdot \rho \cdot V_b \cdot b^2 \cdot \frac{\partial C_l}{\partial \alpha} \cdot \int_0^T \omega^2 \cdot z_0^2 \cdot \cos^2 \omega \cdot t \cdot dt$$

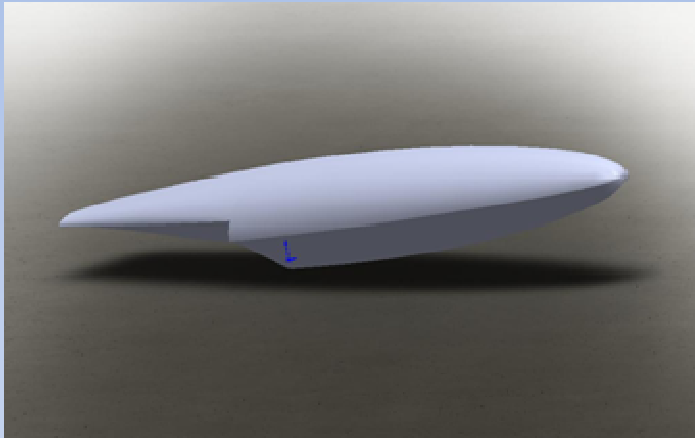
$$\bar{P} = E / T = 0.5 \cdot \rho \cdot b^2 \cdot z_0^2 \cdot \frac{\partial C_l}{\partial \alpha} \cdot V_b \cdot \omega^2 = V_b \cdot D_w$$

$$D_w = \frac{\rho \cdot b^2 \cdot z_0^2 \cdot \omega^2}{4} \left[ \frac{\partial C_l}{\partial \alpha} \right]$$

$$= \rho \left[ \frac{\pi \cdot b \cdot z_0 \cdot V_b \cdot \sin \theta}{\lambda} \right]^2 \left[ \frac{\partial C_l}{\partial \alpha} \right]$$

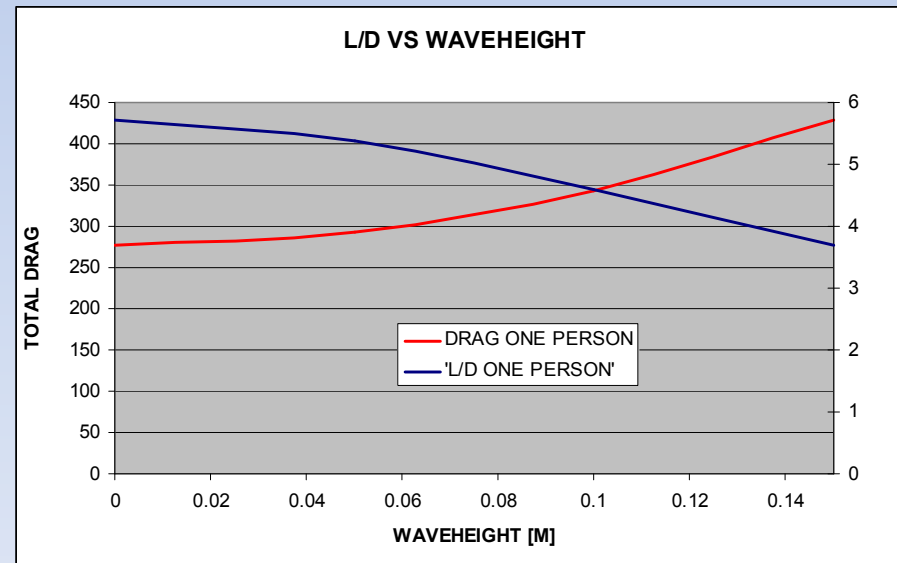


# RESULTS APPLIED TO VSR2 FLOATS



Dimension		
LOA	2.1	m
Beam	0.89	m
Deadrise	19.8	Deg
Total displacement	320	Kg
Design trim	6	Degrees
Step to transom	0.8	M
Normal static payload	127	kg

1. 60% INCREASE IN DRAG IN 150MM WAVES
2. L/D REDUCES FROM 5.8 TO 3.7



# VSR2

- DESIGN OUT THE FAULTS WITH VSR1
- HIGHER TARGET SPEED 60K
- SUPERVENTILATING FOIL
- RAISED AERODYNAMIC FUSELAGE
- CARRY SECOND PERSON
- FEATHERING WING



# LAUNCH MARCH 8 2011



LENGTH	12m
BEAM	10m
MASS	280kg
WING AREA	22m <sup>2</sup>

WING  
EXTENSION

# VSR2



# 40 KNOTS 3<sup>RD</sup> RUN (24/5/2011)

1. NO WING EXTENSION
2. LOW SPEED FOIL
3. TIP NOT SHEETED IN.



50knots is easy - October 2011





# Foil matters

MINIMUM IMMERSED  
SPAN 800MM FOR  
HOOKED IN SECURITY IN  
WAVES



BENDING AT CORNER  
= 1 TONNE X 400MM

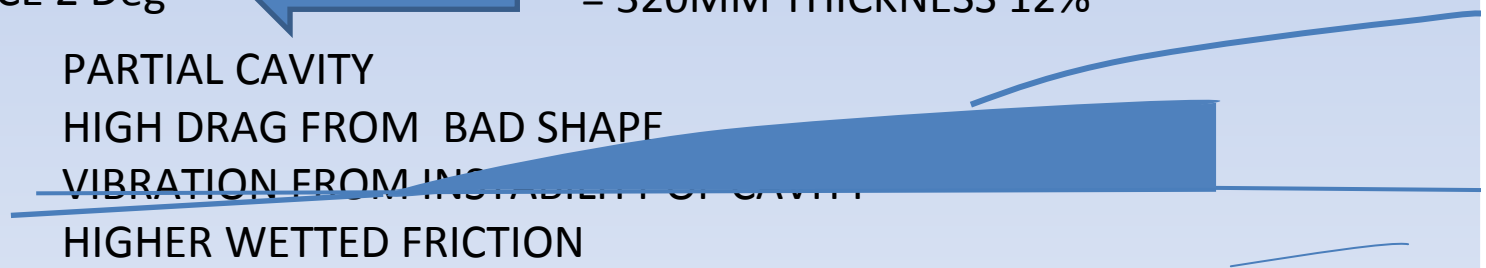
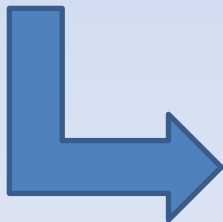


AREA = 0.16m<sup>2</sup>  
CL@50KNOTS = 0.1  
TYPICAL INCIDENCE 2 Deg



CHORD AT CORNER  
= 320MM THICKNESS 12%

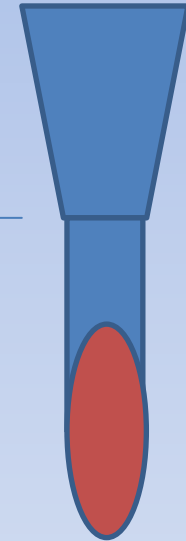
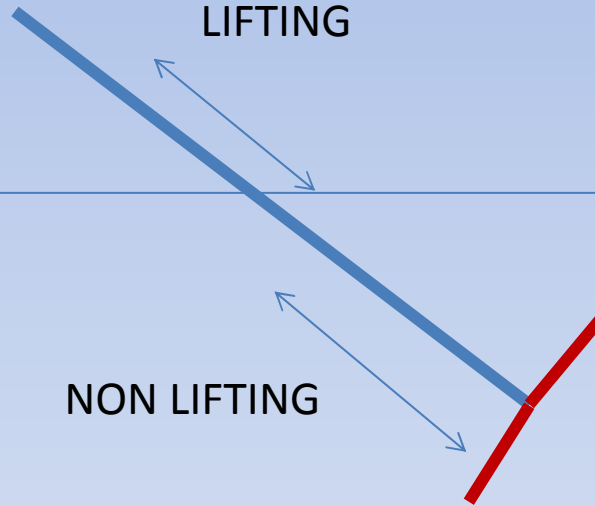
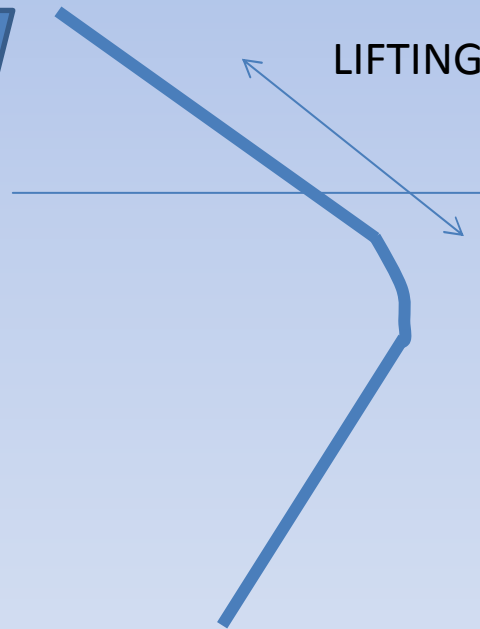
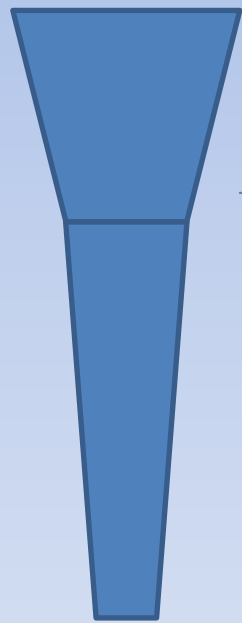
PARTIAL CAVITY  
HIGH DRAG FROM BAD SHAPE  
VIBRATION FROM INSTABILITY OF CAVITY  
HIGHER WETTED FRICTION



CURRENT

SUPERCNAV EVOLUTION

NEXT



# IDEAL FOIL DEVELOPMENT VEHICLE

OPERABLE IN  
30KNOTS



NEAR PERFECT PASSIVE PITCH AND ROLL  
(MANUAL ROLL TRIM AVAILABLE)

EXCELLENT  
DIRECTIONAL  
CONTROL

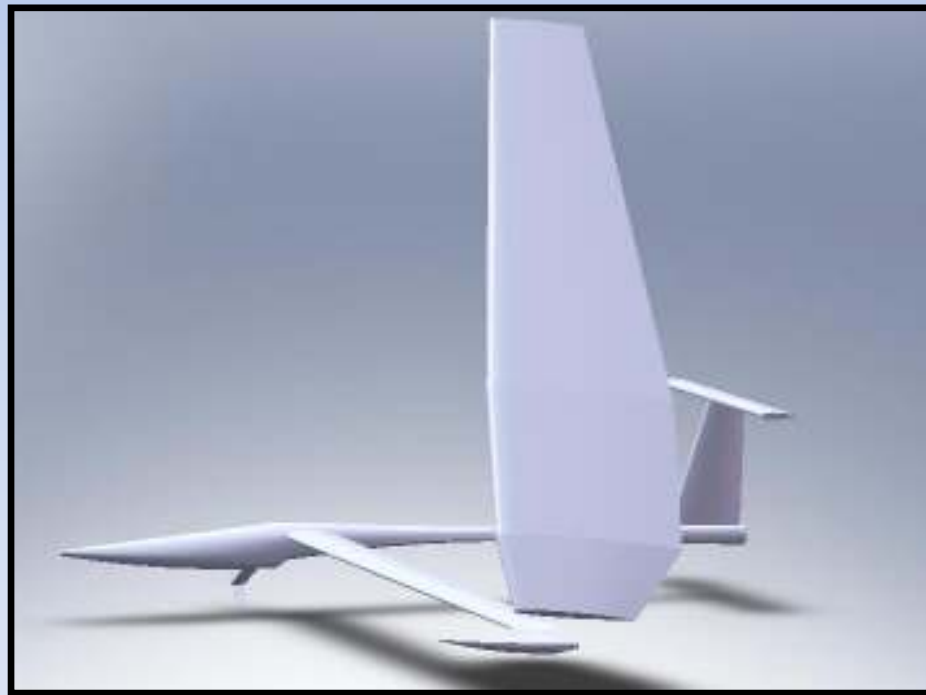


NO STRUCTURAL FAILURES TO DATE

CARRIES 2<sup>ND</sup> PERSON

# THE FUTURE

WHAT WILL THE FASTEST SAILING BOATS LOOK LIKE IN 15 YEARS?



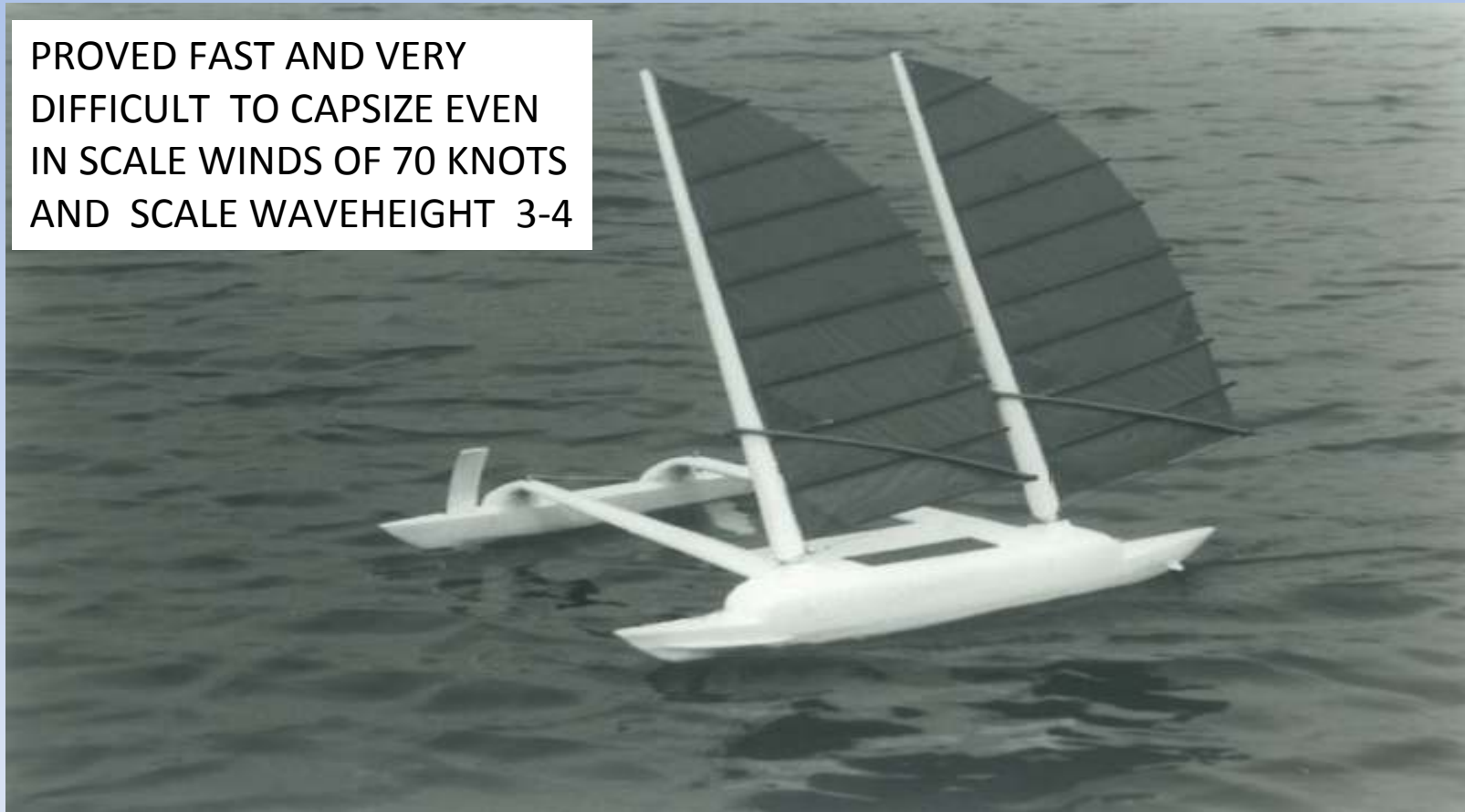
# THE NEW AGE OF PROAS

- SAILING IS AN ASYMMETRIC PROCESS
- THE MOST EFFICIENT DEVICES REFLECT THIS
- SYMMETRIC MULTIHULLS HAVE HIGH REDUNDANCY ON EACH TACK AND HIGH WINDAGE
- THE STRUCTURAL TECHNOLOGY IS NO LONGER AN ISSUE
- 'SMITH' STABILITY IS EASIER TO INTRODUCE
- TACKING TIME IS NOT CRITICAL OFFSHORE

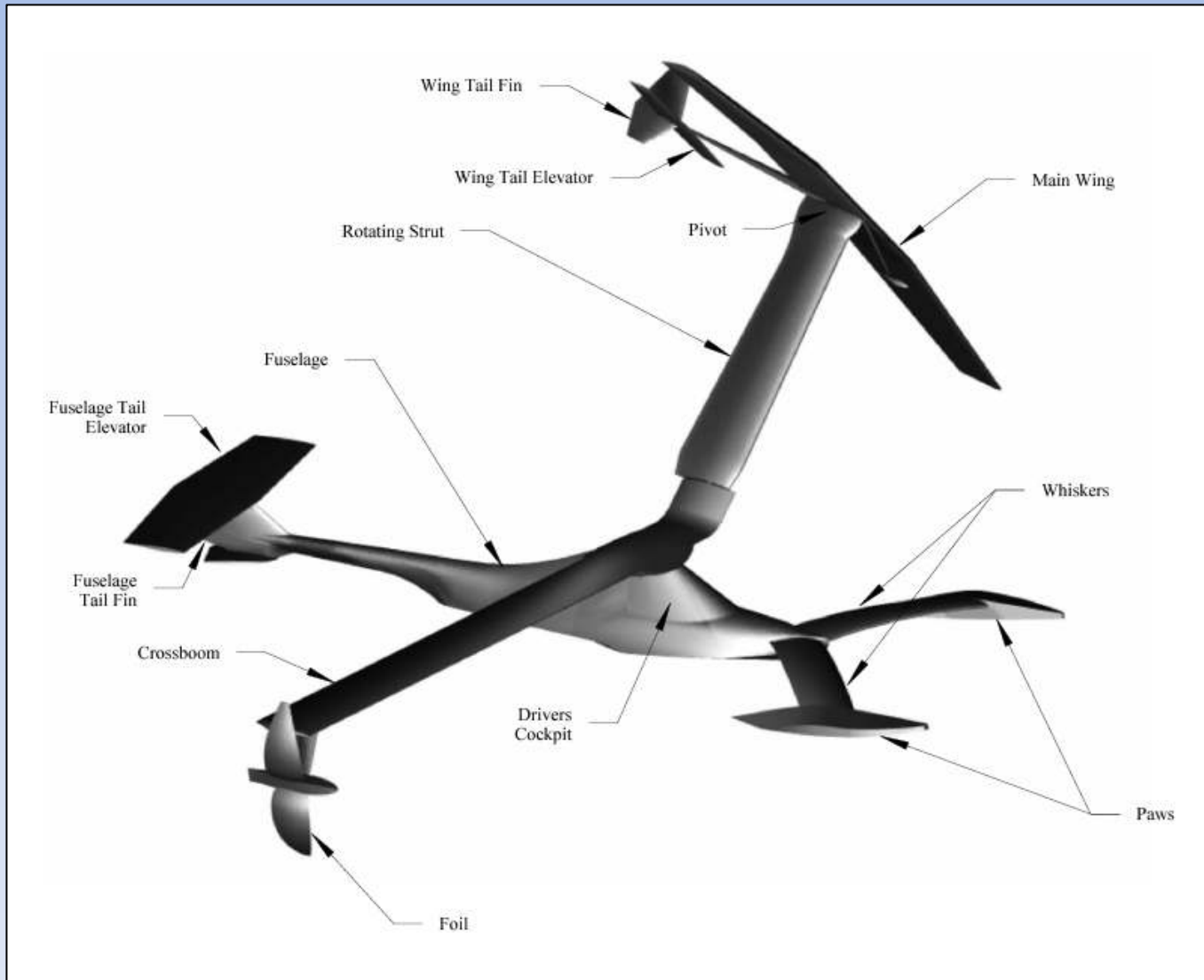


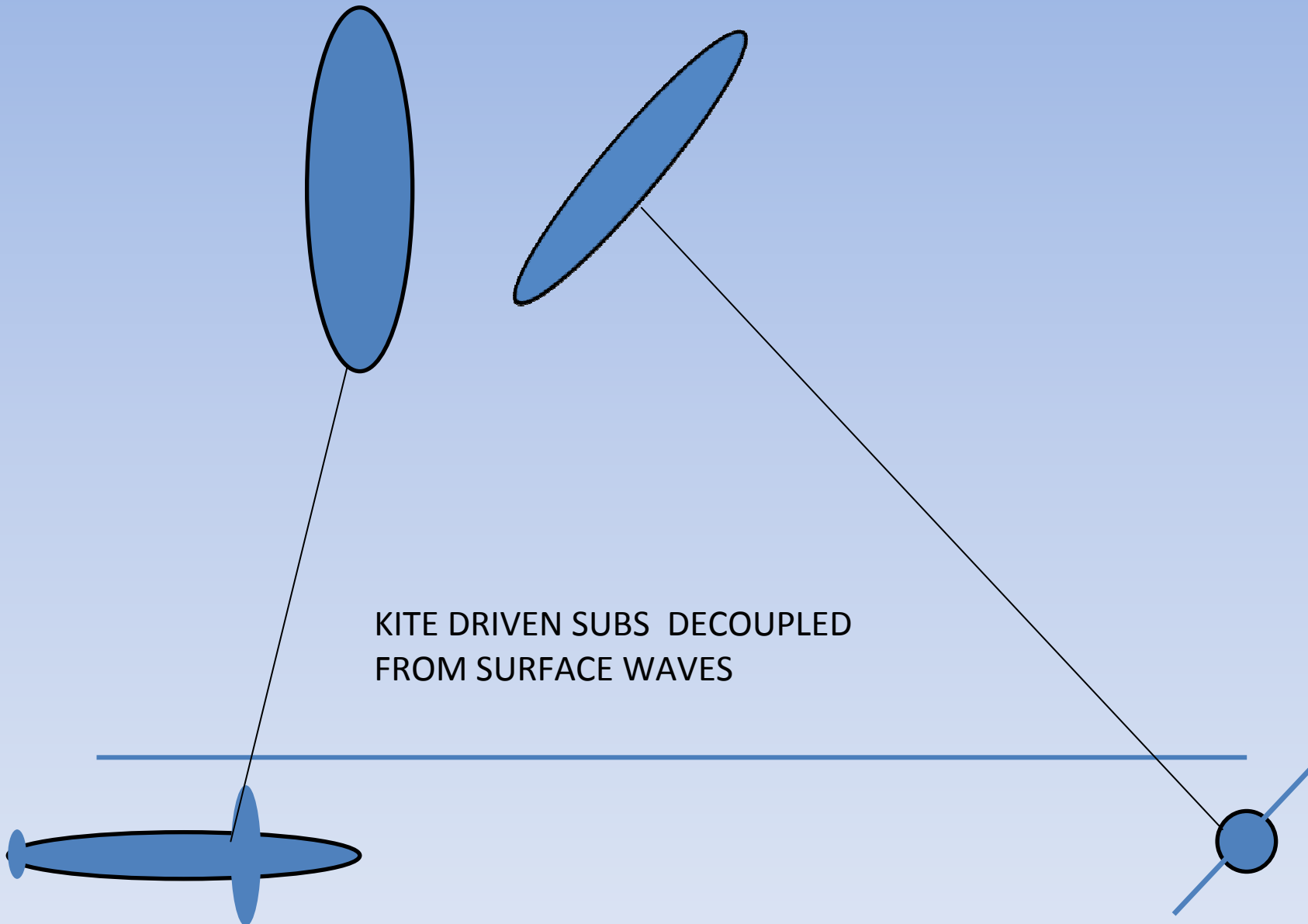
# EXPERIMENTAL SMITH TYPE PROA

PROVED FAST AND VERY  
DIFFICULT TO CAPSIZE EVEN  
IN SCALE WINDS OF 70 KNOTS  
AND SCALE WAVEHEIGHT 3-4



# MONOFOIL - THE FLYING BOAT





KITE DRIVEN SUBS DECOUPLED  
FROM SURFACE WAVES



# 15 YEAR FORECAST

1. KITE POWER WILL BECOME PROMINANT IN MANY VARIED APPLICATIONS , INCLUDING FUEL SAVING ON COMMERCIAL CARGO VESSELS.
2. PROAS WILL GRADUALLY OUTPERFORM TRIMARANS AND CATAMARANS AND BECOME DOMINANT IN RACING ACROSS OCEANS
3. PROAS WILL ADOPT THE 'SMITH' BALANCING CONCEPT TO VARYING DEGREES
4. VARIABLE GEOMETRY WILL BECOME THE NORM
5. THERE WILL BE A RETURN TO LOWER TECH STRUCTURAL SOLUTIONS (EVEN FOR RACING CRAFT)
6. THE WORLD SPEED RECORD WILL REACH 75 KNOTS
7. 24 HOUR AVERAGE OF 50 KNOTS (1200NM)
8. KITE BOARDS WILL REACH THE LOW 60'S KNOTS

# THE FINAL WORD

*The sailboat offends neither fish, fowl nor man. To make it go faster is to make it even more a thing of freedom and beauty'*

*Bernard Smith . The Forty Knot Sailboat 1963*

